

# Sentinel-1 InSAR Capabilities: Results from the Sentinel-1A Commissioning Phase

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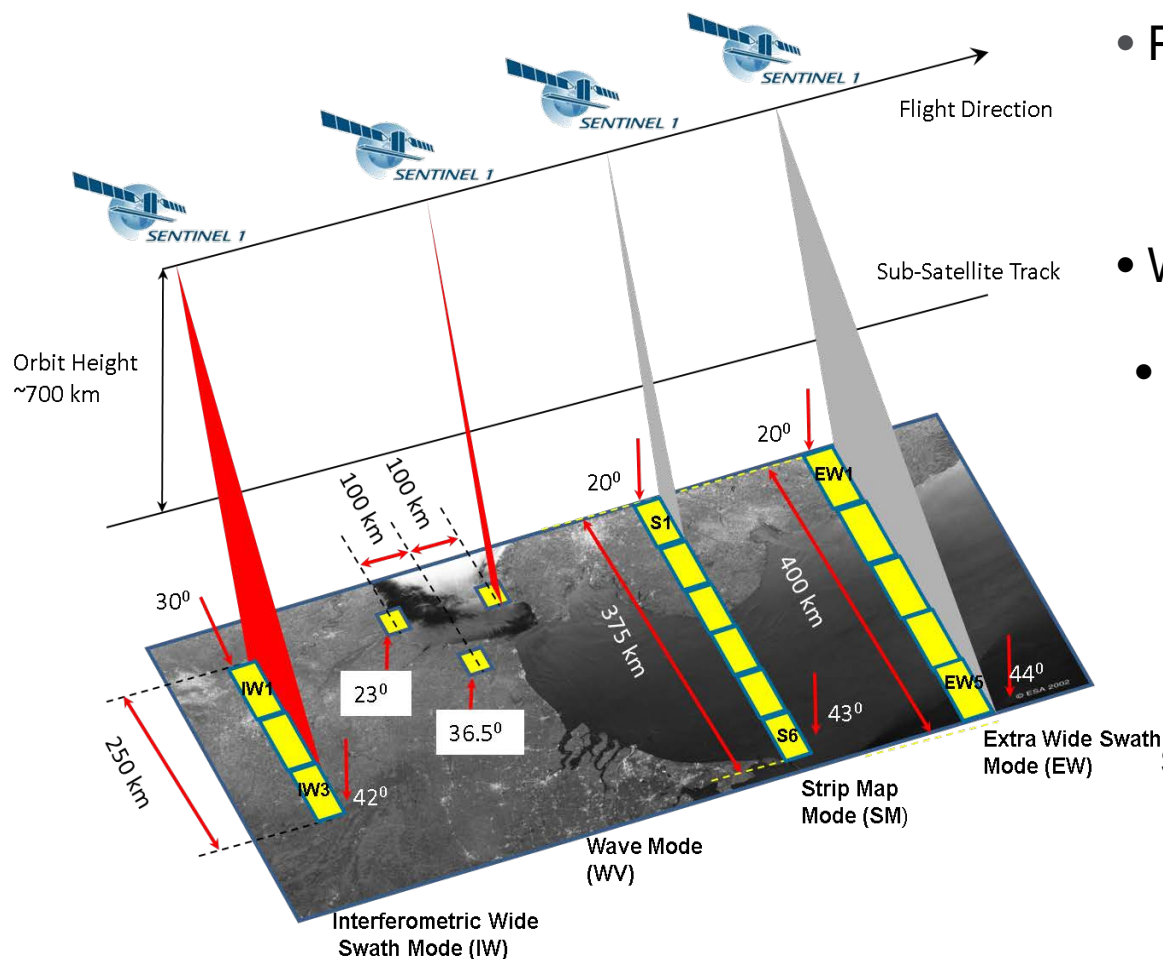
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<sup>3</sup>DLR, Microwave and Radar Institute

<sup>4</sup>Politecnico Di Milano

- SAR Instrument provides 4 exclusive SAR modes with different resolution and coverage



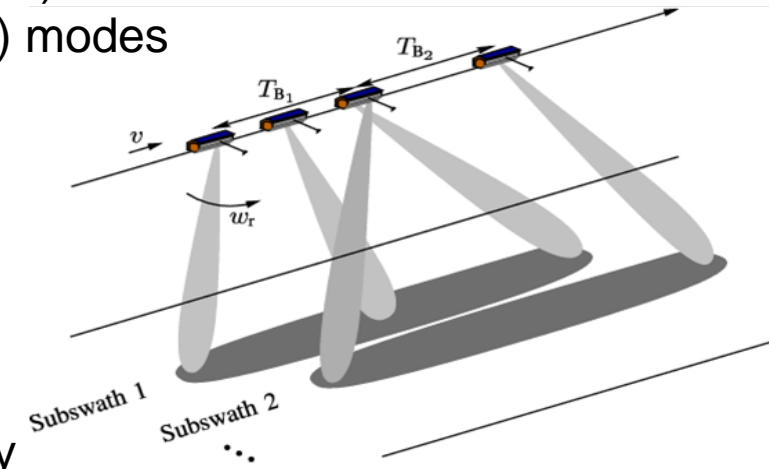
- Polarisation schemes for *IW*, *EW* & *SM*:
  - ✓ single pol: HH or VV
  - ✓ dual pol: HH+HV or VV+VH
- Wave mode (*WV*): HH or VV
- SAR duty cycle per orbit:
  - ✓ up to 25 min in any imaging mode
  - ✓ up to 74 min in Wave mode

Main mode of operations: *Interferometric Wide Swath (IW) mode* satisfies most Copernicus service and user requirements for land & coastal monitoring (i.e. resolution, swath width, polarisation)

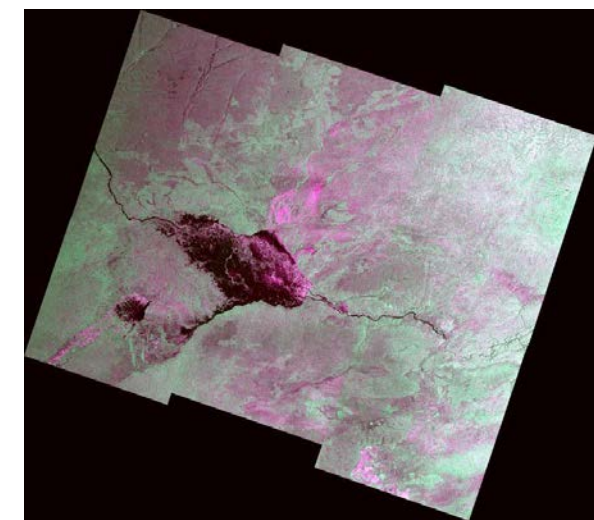
*Wave (WV) mode* is continuously operated over open ocean

TOPS (Terrain Observation with Progressive Scans in azimuth) for Sentinel-1  
*Interferometric Wide Swath (IW)* and *Extra Wide Swath (EW)* modes

- ScanSAR-type beam steering in *elevation* to provide large swath width (IW: 250km and EW: 400km)
- Antenna beam is steered along *azimuth* from *aft* to the *fore* at a constant rate
- ✓ All targets are observed by the entire azimuth antenna pattern *eliminating scalloping effect* in ScanSAR imagery
- ✓ *Constant SNR* and *azimuth ambiguities*
- ✓ Reduction of azimuth resolution due to decrease in dwell time
- S-1 IW TOPS mode parameters:  
 $\pm 0.6^\circ$  azimuth scanning at Pulse Repetition Interval rate with step size of 1.6 mdeg.



Sentinel-1A IW dual-pol image,  
acquired over Namibia



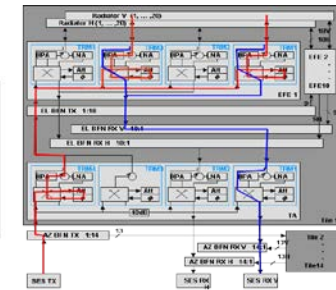
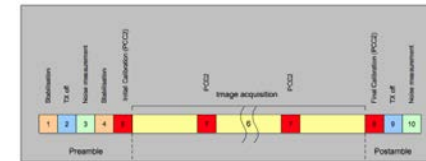
# Sentinel-1 SAR System Calibration and Performance Verification



- Verification of in-orbit SAR system performance & monitoring of stability (temperature)

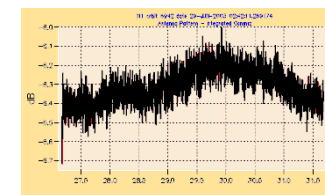
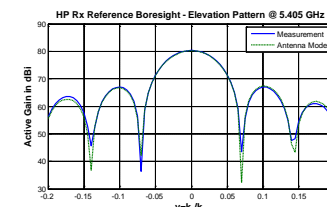
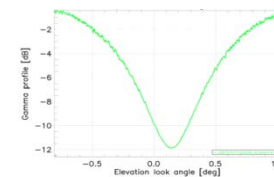
## Internal Calibration

- Network of Cal pulses monitors potential drifts in the instrument's Tx & Rx signal paths + entire antenna system (T/R modules)
  - Monitoring of instrument stability over time & vs. temperature
  - Thermal system noise characterization
  - Inter-channel gain and phase characterization
  - Internal instrument delay characterization
  - TRM and EFE drift characterization based upon RFC mode



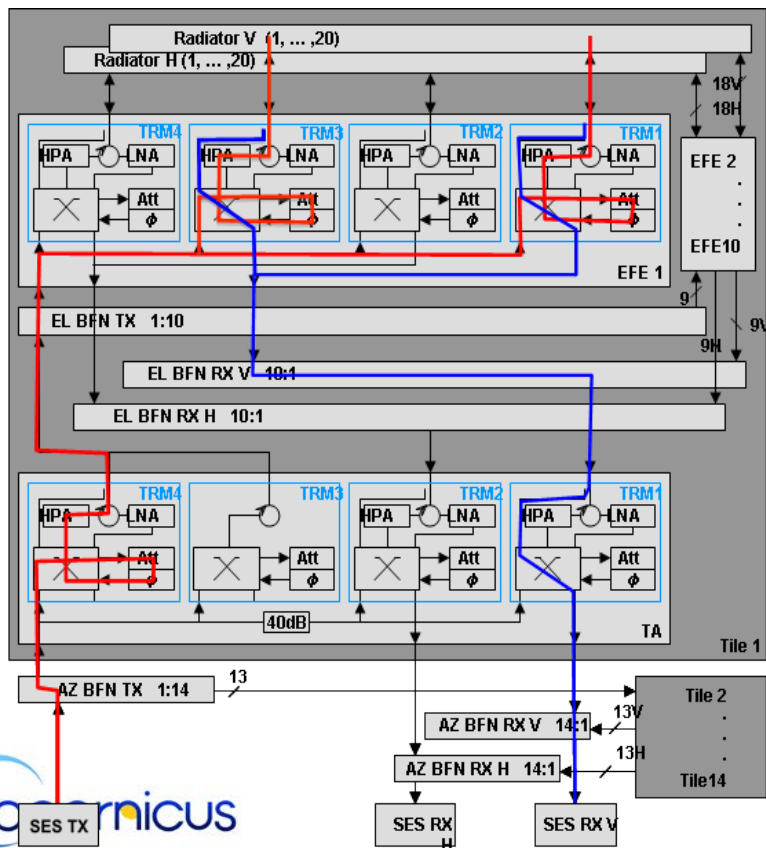
## External Calibration

- Measurement of SAR system w.r.t. reference targets with known *radar cross section* (RCS)
- Absolute radiometric calibration ( $< 1$  dB ( $3\sigma$ )) and stability ( $< 0.5$  dB ( $3\sigma$ ))
- Antenna pointing calibration ( $< 0.01^\circ$ )
- Antenna Model verification (0.2 dB ( $3\sigma$ ) for 2-way gain)
- Geometric calibration (pixel localization: 2.5m ( $3\sigma$ ))
- Interferometric verification
- Polarimetric calibration

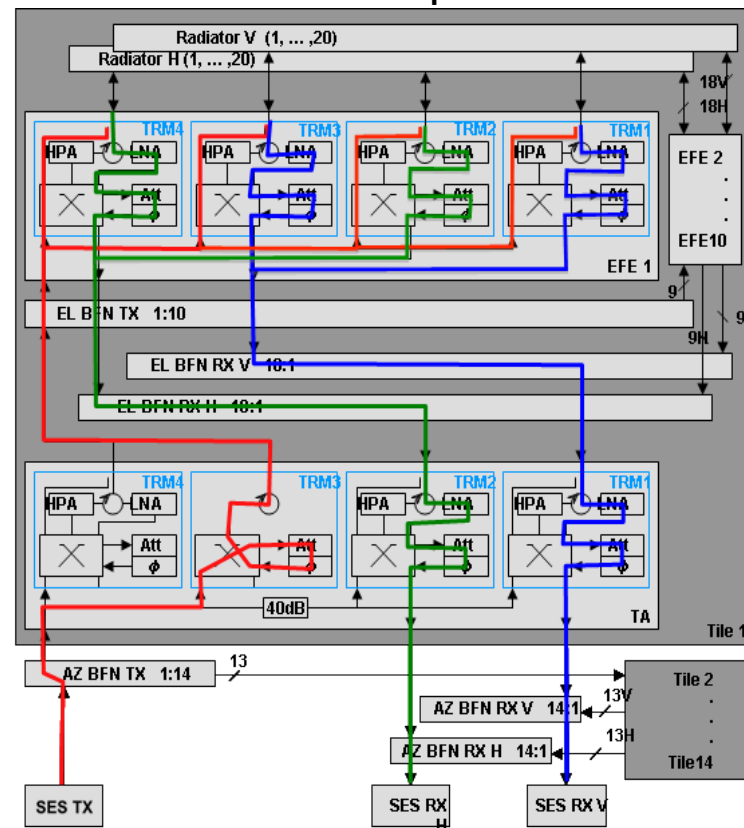


- Network of Cal pulses monitors potential drifts in instrument's Tx and Rx signal paths except for:
  - Antenna radiators (covered by Antenna Model)
  - Calibration couplers and calibration paths (strict stability requirements)

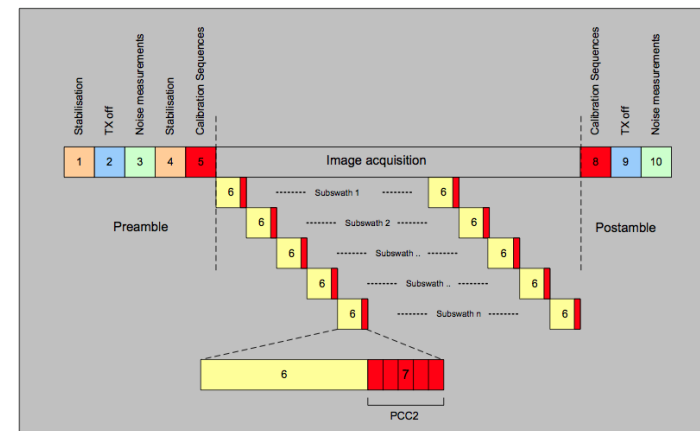
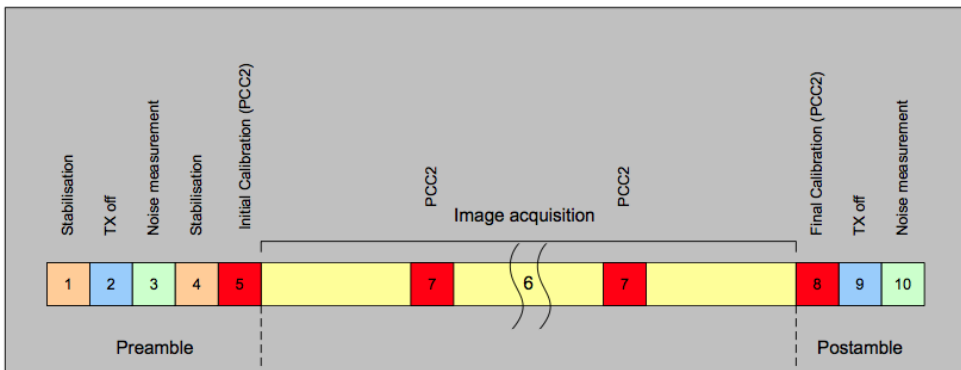
### TxCal (V) single-pol



### RxCal dual-pol



- Each DT starts and ends with sequences of 6 types of Cal pulses both at nominal signal BW and at 100MHz BW (400 PRIs required):
  - 4 PCC2 phase-coded pulses (RxCal, TxCal, EPDNCaI, TACaI)
  - 2 non phase-coded (TxCalHlso, APDNCaI)



- Cal pulses are used in ground processing for gain and phase, i.e. PG product correction

$$PG = \frac{TxCal \cdot RxCal}{EPDNCaI} \frac{TACaI}{APDNCaI}$$

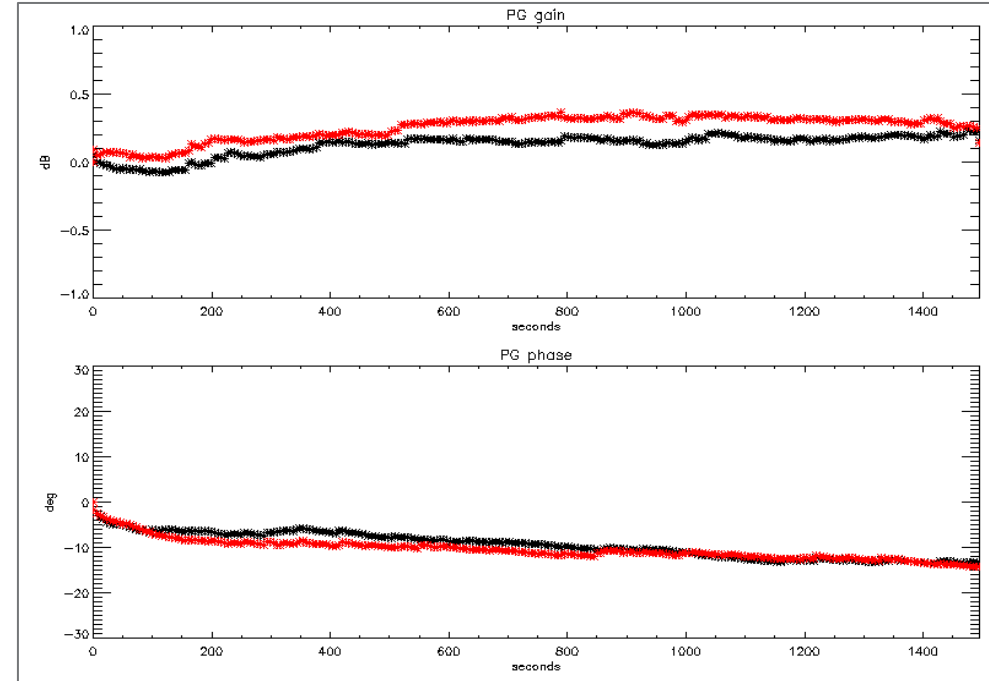
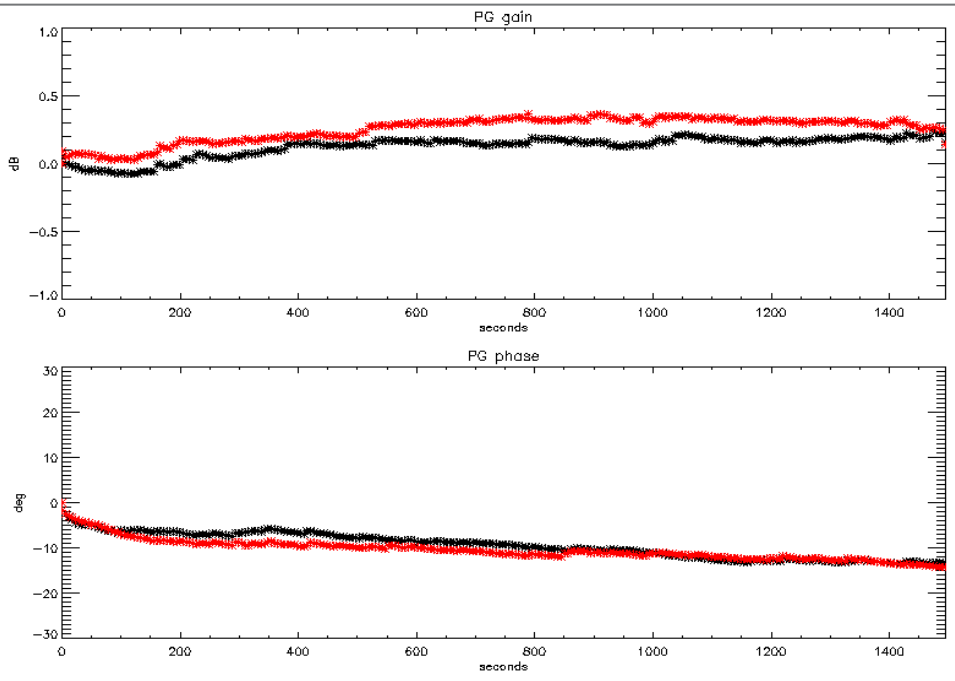
Product (complex) of Transmit power and Receive gain

# Sentinel-1A Instrument stability during long datatakes



## Interferometric Wide Swath Mode

## Stripmap 6



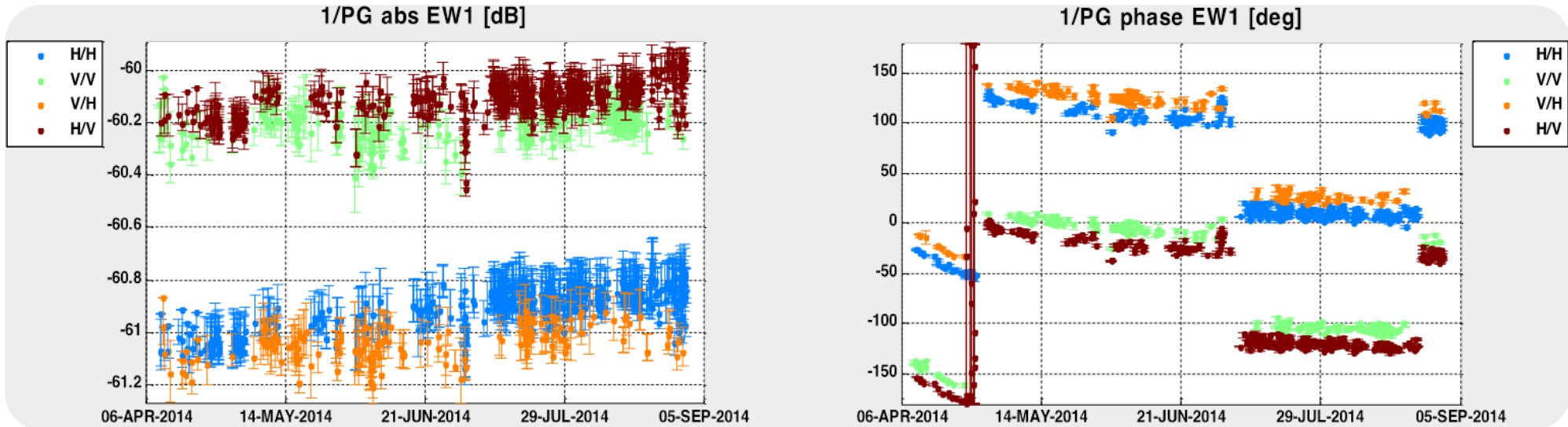
### Variation over 25 min:

Gain	0.31 dB (VV) 0.37 dB (VH)
Phase	-13.6° (VV) -14.3° (VH)

### Variation over 21 min

Gain	0.32 dB (VV) 0.43 dB (VH)
Phase	-14.0° (VV) -14.7° (VH)

# Sentinel-1A Instrument stability over 5 months



- Variations in amplitude  $<0.6$  dB in 150 days
- Discrete jumps in phase and internal delay occur when the SES is restarted
- Amplitude and phase variations are tracked by internal calibration and compensated for by the operational SAR processor (IPF)



Measurement of *Range-Doppler geolocation* of known reference Point target in SAR image for estimation of *systematic SAR timing offsets* in:

- *slant range* (residual internal electronic path delay and Sample Window Start Time)
- *azimuth* (radar time and spacecraft GPS time)

⇒ **Absolute Location Error (ALE) = predicted – measured (PTs)**

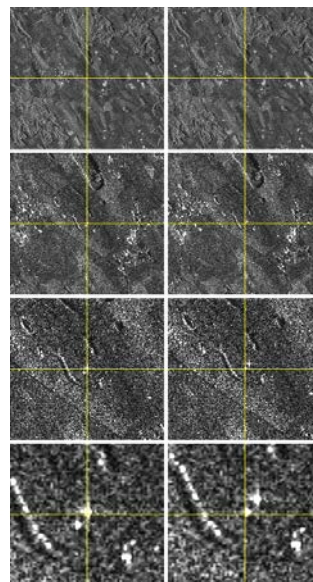
Geolocation accuracy may be affected by:

- Spacecraft position (orbital state vectors) accuracy
- Survey accuracy of reference target
- Atmospheric path delay of radar signal

Cross-hair prediction depends on orbit data type

## **Reference Point Targets (PTs)**

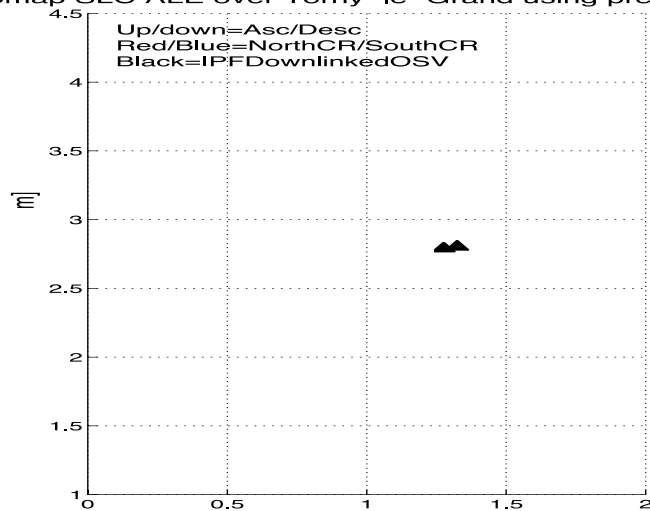
- 4 corner reflectors (CRs) deployed at Torny-le-Grand, Switzerland
- 3 ESA transponders deployed in the Netherlands



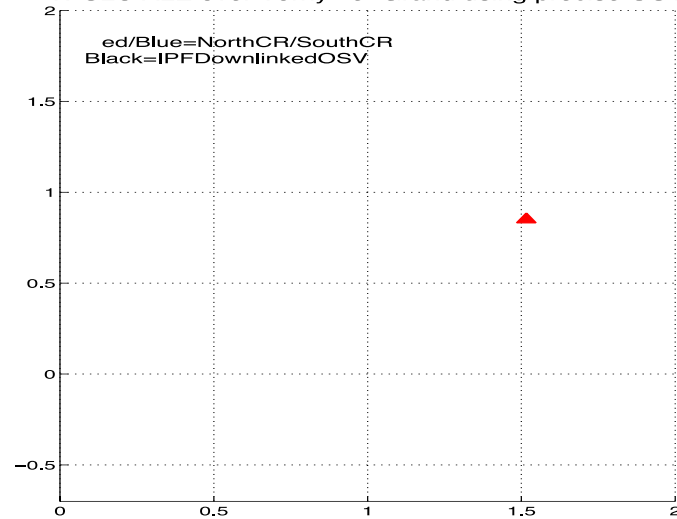
Data analyzed over **Torny-le-Grand** corner reflector site by University of Zurich, RSL

- 19 SM and 3 IW and use of *Precise Orbit Data (POD)*

Stripmap SLC ALE over Torny-le-Grand using precise OSVs



IW SLC ALE over Torny-le-Grand using precise OSVs



## Applied corrections:

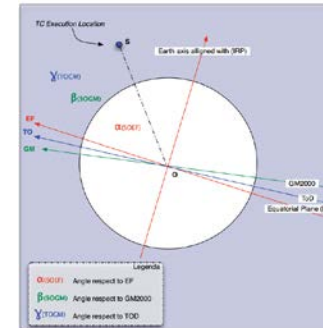
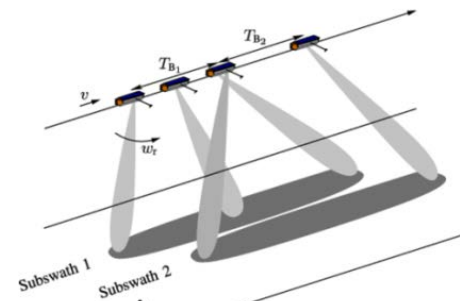
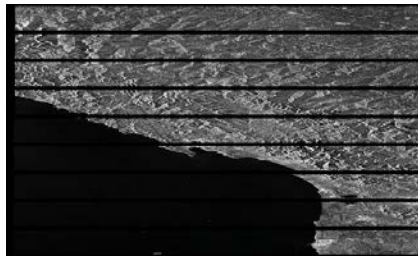
- Internal path delay
- Tectonic motion
- Solid Earth tides motion
- Atmospheric path delay

	ALE Slant range offset		ALE Azimuth offset	
<b>SM</b>	$1.28 \pm 0.07$ m	$8 \times 10^{-9}$ sec	$2.09 \pm 0.49$ m	$3.08 \times 10^{-4} \pm 6.79 \times 10^{-5}$ sec
<b>IW</b>	$1.31 \pm 0.37$ m	$8 \times 10^{-9}$ sec	$0.53 \pm 0.74$ m	$7.7 \times 10^{-5} \pm 1.1 \times 10^{-4}$ sec

**Recommendation:** Annotate *slant range time delay* in SAR image data products

# SAR Interferometry (InSAR) Verification

Repeat-pass TOPS InSAR using **Interferometric Wide Swath (IW)** data pairs worked on the 'spot'



**Burst synchronization**

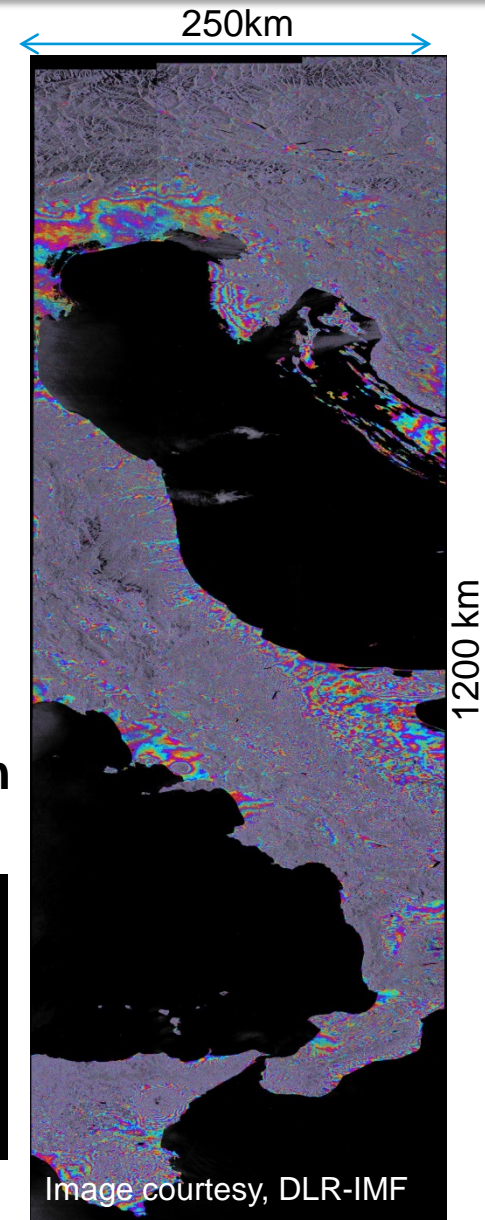
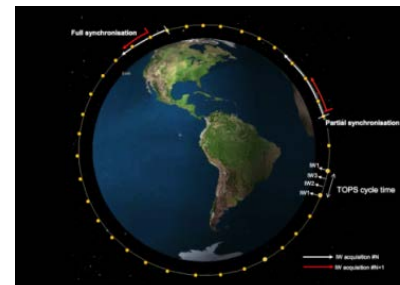
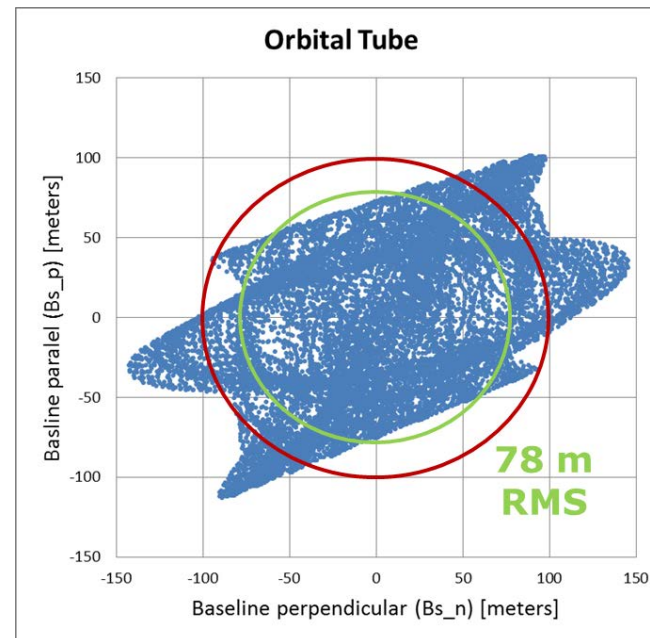
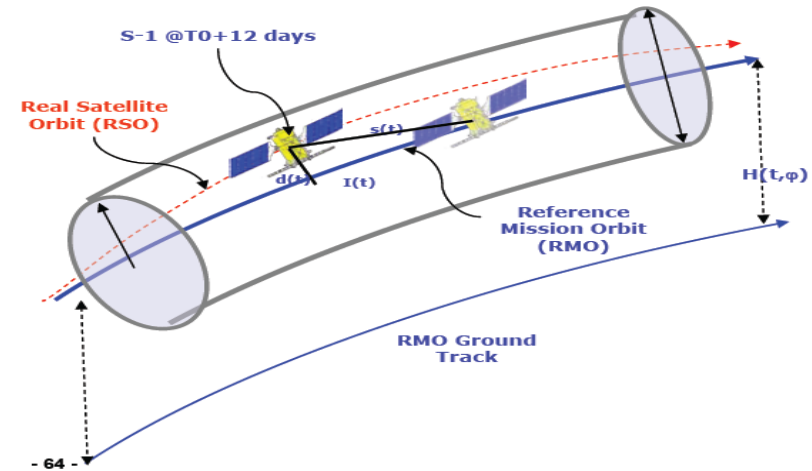


Image courtesy, DLR-IMF

Provides ultimate verification of:

- SAR instrument phase stability (over repeat orbit cycles)
- Satellite on-board timing and GNSS solution to support *position-tagged commanding* (OPS angle)
- Accurate orbit control and maintenance (orbital tube)
- Mission Planning system using *TOPS cycle time grid points* for data take start time estimation
- IPF produces phase-preserving Level-1 SLC product slices

- Reference orbit was reached on August 7<sup>th</sup>, 2014
- Satellite will be kept within an *Orbital Tube* around a *Reference Mission Orbit* (RMO)
- Specified *Orbital Tube* radius of 50 (rms)  
⇒ equivalent to ground-track dead band of 60m
- During S-1A Commissioning:  
Relaxation of ground-track dead band to 120m  
⇒ *Orbital Tube* radius of roughly 100 (rms)

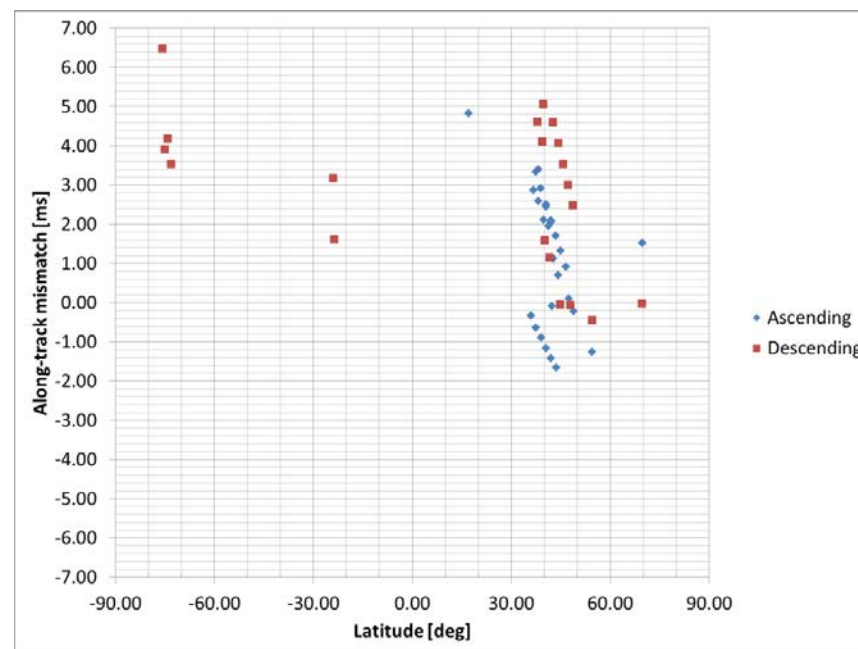
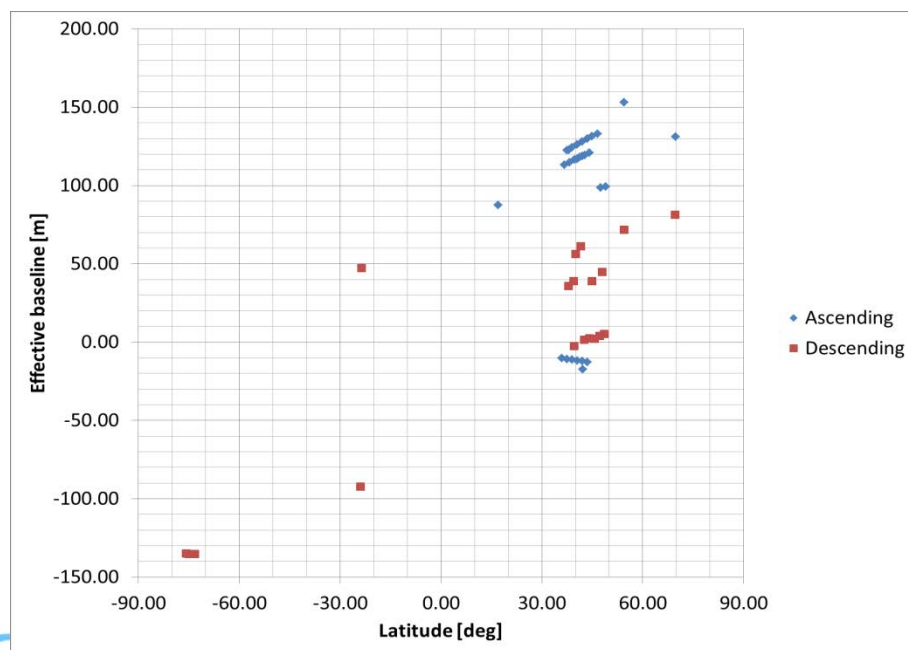


- 48 InSAR product pairs
- 28 ascending geometry
  - 20 descending geometry
  - 46 in IW mode
  - 2 in EW mode



Along-track(burst) mis-synchronization < 2.83ms

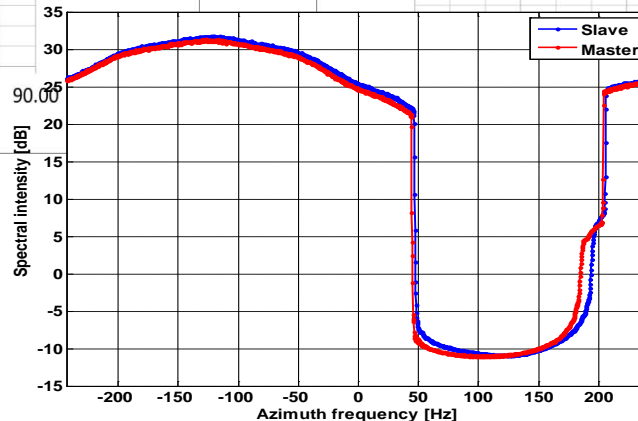
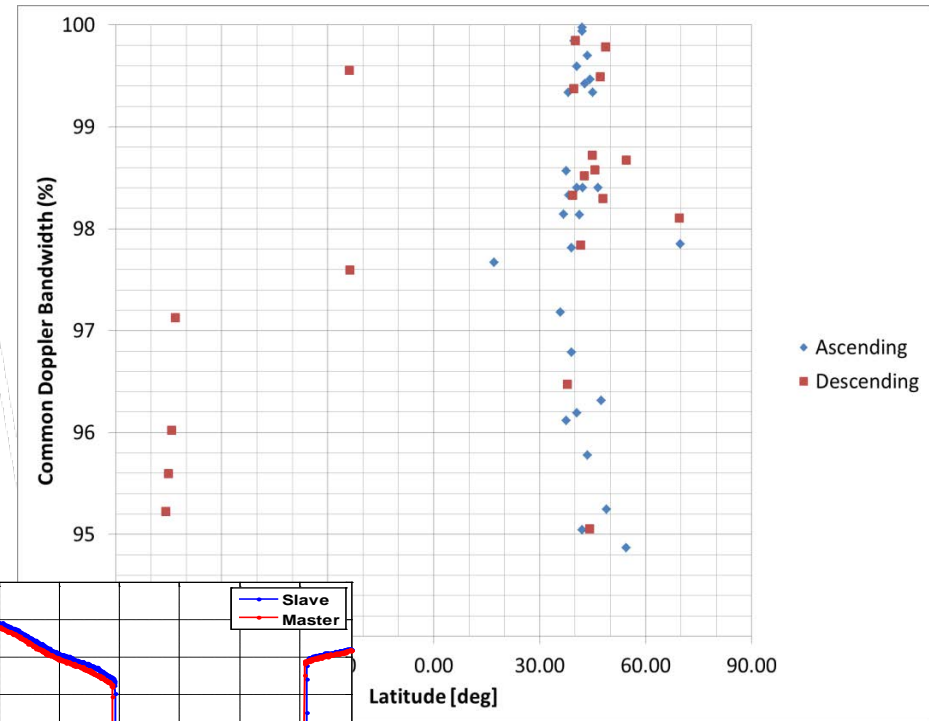
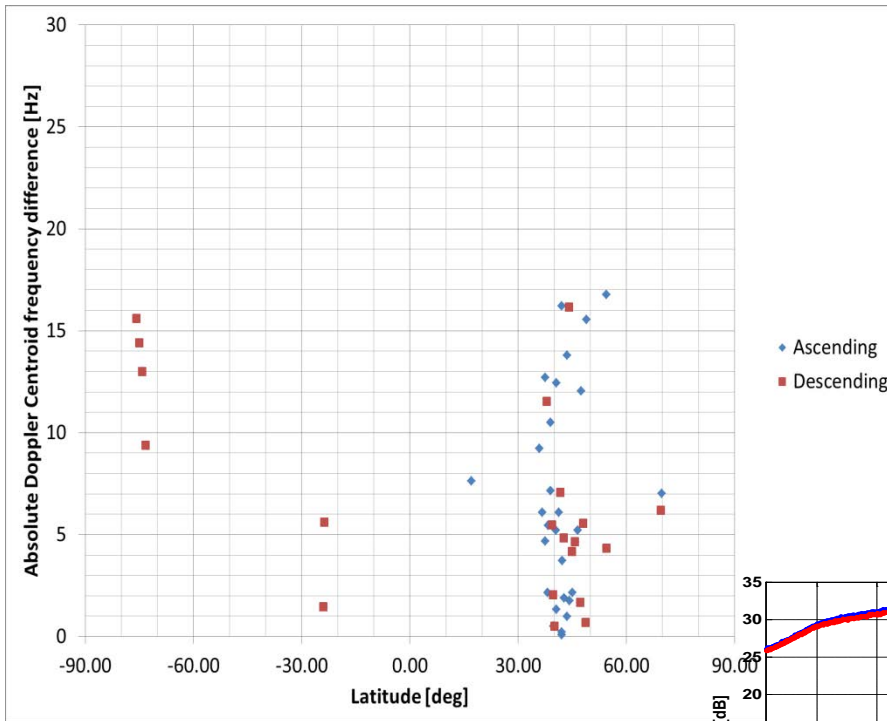
Orbital InSAR baseline of < 150m



	Ascending	Descending
Mean AT mismatch [ms]	1.17	2.83
Stdev AT mismatch [ms]	1.71	1.97

**Doppler centroid difference < 20 Hz**  
stable attitude and antenna pointing

**Common InSAR Doppler bandwidth > 95%**  
of available azimuth bandwidth



## Demonstration of *Differential* and *Multi-Aperture (Squint)* SAR Interferometry

M6.0 South Napa Valley earthquake on August 24<sup>th</sup>, 2014

Use of Stripmap (SM-1) data pairs acquired on August 7<sup>th</sup> and 31<sup>st</sup>, 2014

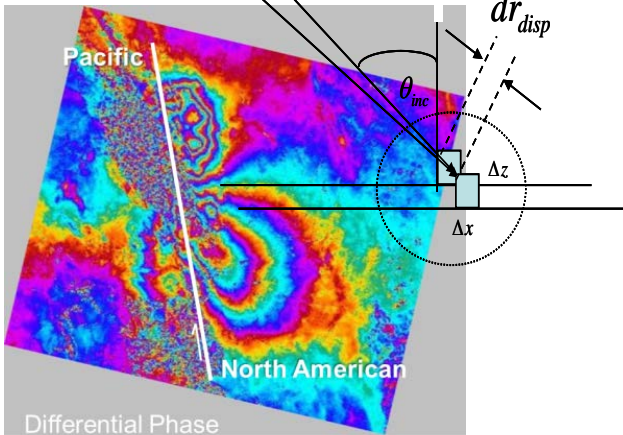
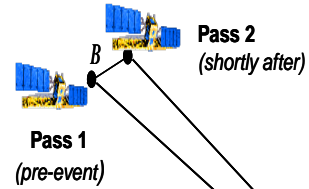
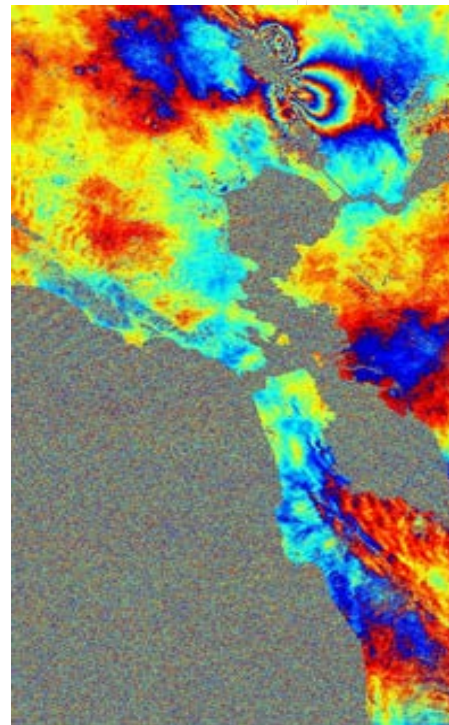


Image courtesy, DLR-IMF

D-InSAR



MAI (MS-InSAR)

